

Background

Over the last decade, autonomous Unmanned Aerial Vehicles (UAVs or "drones") have seen increased usage in industrial, research, and academic applications. They are appealing for commercial or military tasks such as precision agriculture, search and rescue, surveillance, surveying, and film making where the position of the UAV needs to be highly controllable. Quadrotor UAV flight dynamics are a highly nonlinear, strongly coupled, and unstable; Quadrotors are also underactuated systems. This makes developing precision control systems a particularly challenging task.

Therefore, an optimal control law has been developed to advance the state of the art in position control of multirotor UAV's. A Nonlinear Model Predictive Position Controller (NMPC) was developed A weighted basis function method of optimization is introduced to reduce the computational

complexity of the NMPC algorithm. Simulation results show the feasibility of such a being control law implemented on a prototype UAV.

$\ddot{\phi} = b_1 U_2 + a_1 \dot{\theta} \dot{\psi} - a_2 \dot{\theta} \Omega_r + \Gamma_{\phi}(X, u, t, F_d)$	(1)
$\ddot{\theta} = b_2 U_3 + a_3 \dot{\phi} \dot{\psi} + a_4 \dot{\phi} \Omega_r + \Gamma_{\theta} (X, u, t, F_d)$ Attitude	(2)
$\ddot{\psi} = b_3 U_4 + a_5 \dot{\phi} \dot{\theta} + \Gamma_{\psi}(X, u, t, F_d)$	(3)
$\ddot{x} = \frac{U_1}{m}(\sin\phi\sin\psi + \cos\phi\cos\psi\sin\theta) + \Gamma_x(X, u, t, F_d)$	(4)
$\ddot{y} = \frac{U_1}{m}(\cos\phi\sin\psi\sin\theta - \cos\psi\sin\phi) + \Gamma_y(X, u, t, F_d)$	(5)
$\ddot{z} = \frac{U_1}{m}(\cos\phi\cos\theta) - g + \Gamma_z(X, u, t, F_d)$ Position	(6)

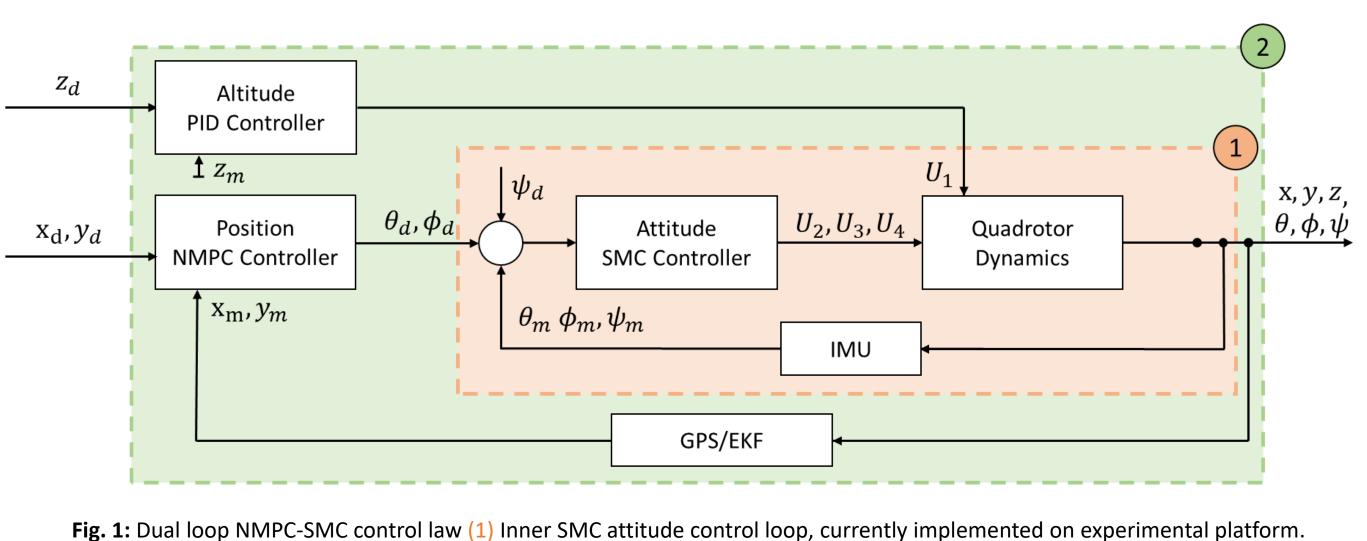
Equation 1: Quadrotor Dynamics

Control Law Outline

The dual loop controller applying SMC and NMPC is shown in Figure 1. In this configuration, the position controller provides setpoints to the attitude controller which in turn actuates the system. Sliding mode is ideal for the inner attitude loop since it is robust enough to account for unmodeled dynamics and deficient actuators.

NMPC is based on an iterative optimization of a set of control inputs over a finite prediction horizon – a finite window of time in the future. It is capable of finding an exact solution to a trajectory tracking control problem for a predefined, desired trajectory.

The NMPC-SMC dual loop controller is expected to provide precise control over the UAV position and attitude dynamics, and can be applied to quadrotor research platforms used for spacecraft simulation.



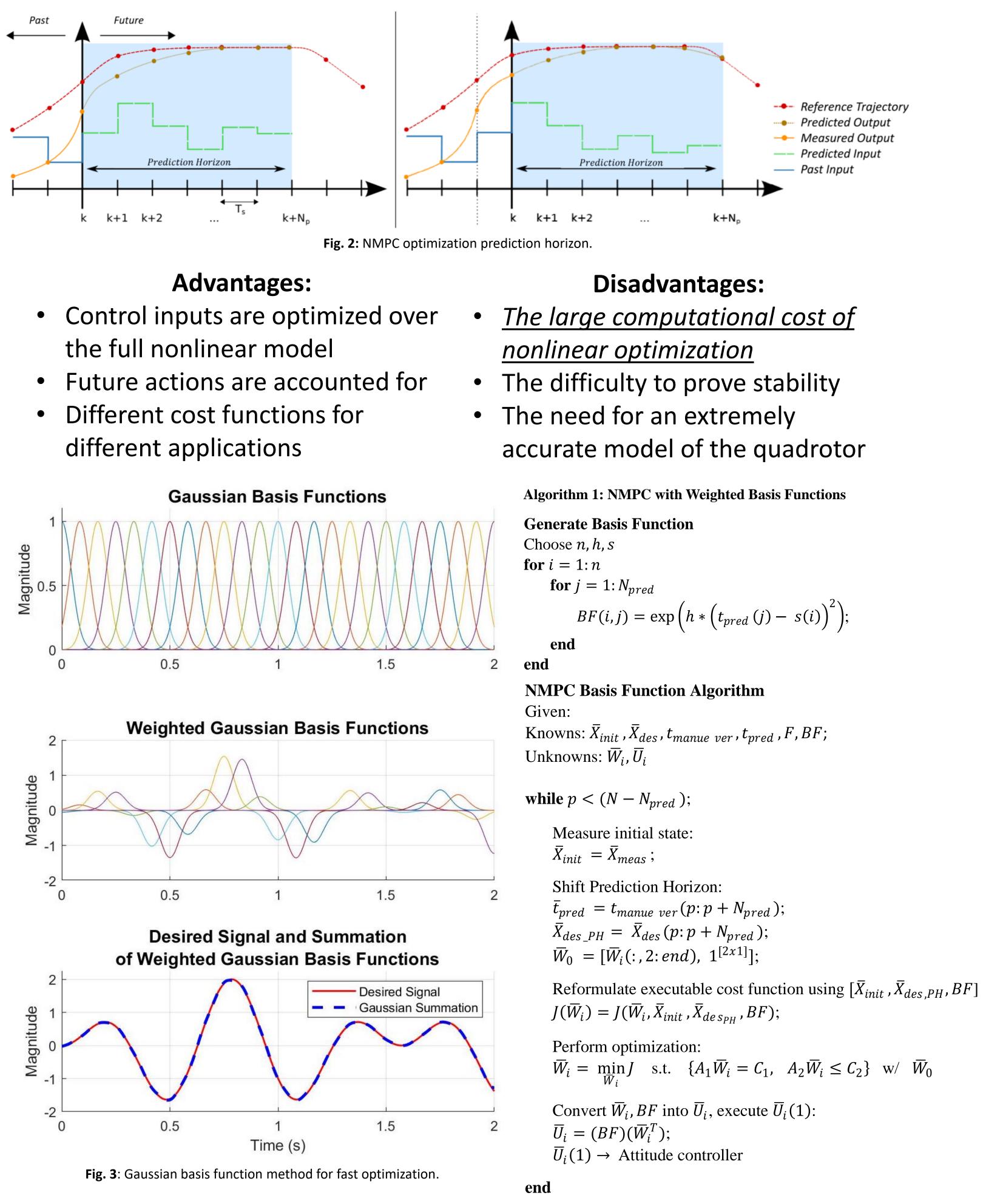
(2) Outer NMPC position control loop, developed in simulation.

Improved Multirotor UAV Flight Controller using **Nonlinear Model Predictive Position Control Andrew Masters**

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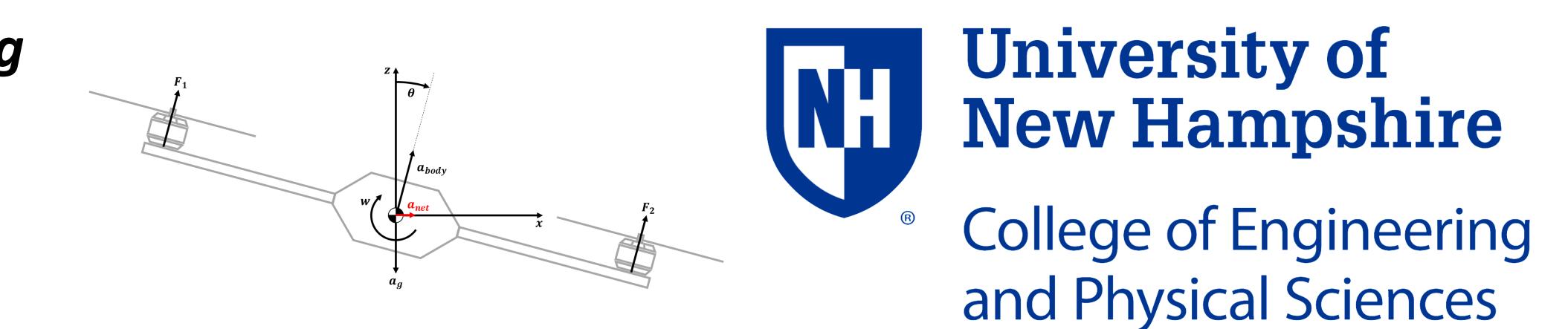
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NMPC with Weighted Basis Functions

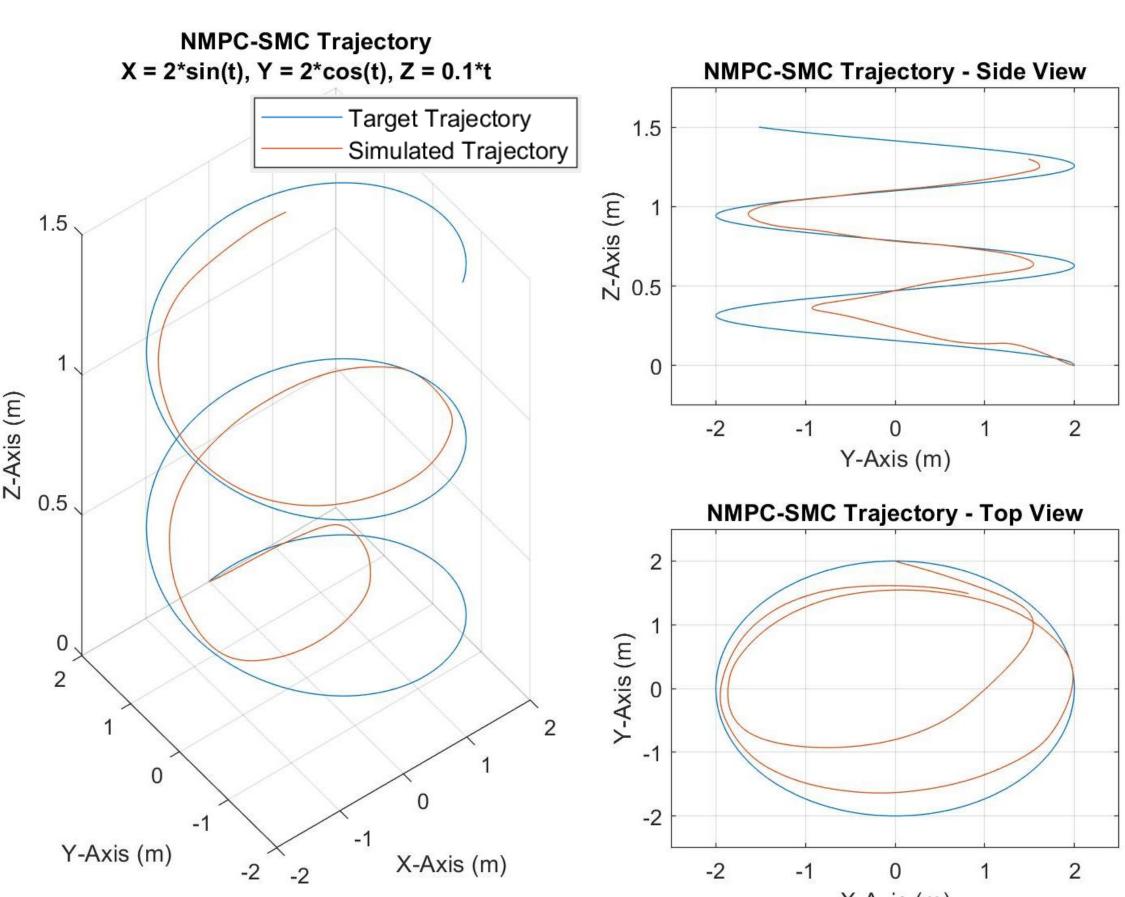


$$J = \left[\sum_{i=1}^{N_{pred}} |X_{des}(i) - X_{meas}(i)| + |Y_{des}(i) - X_{meas}(i)| \right] + \left[Y_{des}(i) - X_{meas}(i) - X_{meas}(i) - X_{meas}(i) \right] + \left[Y_{des}(i) - X_{meas}(i) - X_{meas}(i) - X_{meas}(i) - X_{meas}(i) - X_{meas}(i) \right] + \left[Y_{des}(i) - X_{meas}(i) - X_{meas}(i) - X_{meas}(i) - X_{meas}(i) - X_{meas}(i) \right] + \left[Y_{des}(i) - X_{meas}(i) - X_{meas}(i) - X_{meas}(i) - X_{meas}(i) - X_{meas}(i) \right] + \left[Y_{des}(i) - X_{meas}(i) - X_{meas}(i) - X_{meas}(i) - X_{meas}(i) - X_{meas}(i) \right] + \left[Y_{des}(i) - X_{meas}(i) - X_{meas}(i) - X_{meas}(i) - X_{meas}(i) - X_{meas}(i) - X_{meas}(i) \right] + \left[Y_{des}(i) - X_{meas}(i) - X_{meas}(i) - X_{meas}(i) - X_{meas}(i) - X_{meas}(i) \right] + \left[Y_{des}(i) - X_{meas}(i) - X_{meas}(i) - X_{meas}(i) - X_{meas}(i) - X_{meas}(i) - X_{meas}(i) \right] + \left[Y_{des}(i) - X_{meas}(i) - X_{meas}(i) - X_{meas}(i) - X_{meas}(i) - X_{meas}(i) \right] + \left[Y_{des}(i) - X_{meas}(i) - X_{meas}(i) - X_{meas}(i) - X_{meas}(i) - X_{meas}(i) \right] + \left[Y_{des}(i) - X_{meas}(i) - X_{meas}(i) - X_{meas}(i) - X_{meas}(i) - X_{meas}(i) \right] + \left[Y_{des}(i) - X_{meas}(i) - X_{meas}(i) - X_{meas}(i) - X_{meas}(i) - X_{meas}(i) \right] + \left[Y_{des}(i) - X_{meas}(i) - X_{meas}(i) - X_{meas}(i) - X_{meas}(i) - X_{meas}(i) \right] + \left[Y_{des}(i) - X_{meas}(i) - X_{meas}(i) - X_{meas}(i) - X_{meas}(i) - X_{meas}(i) \right] + \left[Y_{des}(i) - X_{meas}(i) - X_{meas}(i) - X_{meas}(i) - X_{meas}(i) - X_{meas}(i) - X_{meas}(i) \right] + \left[Y_{meas}(i) - X_{meas}(i) - X_{meas}(i) - X_{meas}(i) - X_{meas}(i) - X_{meas}(i) \right] + \left[Y_{meas}(i) - X_{meas}(i) - X_{meas}(i) - X_{meas}(i) - X_{meas}(i) \right] + \left[Y_{meas}(i) - X_{meas}(i) - X_{meas}(i) - X_{meas}(i) - X_{meas}(i) \right] + \left[Y_{meas}(i) - X_{meas}(i) - X_{meas}(i) - X_{meas}(i) - X_{meas}(i) \right] + \left[Y_{meas}(i) - X_{meas}(i) - X_{meas}(i) - X_{meas}(i) - X_{meas}(i) \right] + \left[Y_{meas}(i) - X_{meas}(i) - X_{meas}(i) - X_{meas}(i) - X_{meas}(i) \right] + \left[Y_{meas}(i) - X_{meas}(i) - X_{meas}(i) - X_{meas}(i) \right] + \left[Y_{meas}(i) - X_{meas}(i) - X_{meas}(i) - X_{meas}(i) \right] + \left[Y_{meas}(i)$$

By taking advantage of the quadrotor's generally sinusoidal angular inputs, basis function can be developed to approximate these input signals using far less optimization parameters. Using this method with a two second prediction horizon at 50Hz, the quadrotor NMPC optimization is reduced from 200 to 20 parameters.



 $-Y_{meas}(i)||+|\sum_{i=1}^{\infty}|\dot{\theta}(i)|+|\dot{\phi}(i)||$ Equation 2: NMPC Cost Function



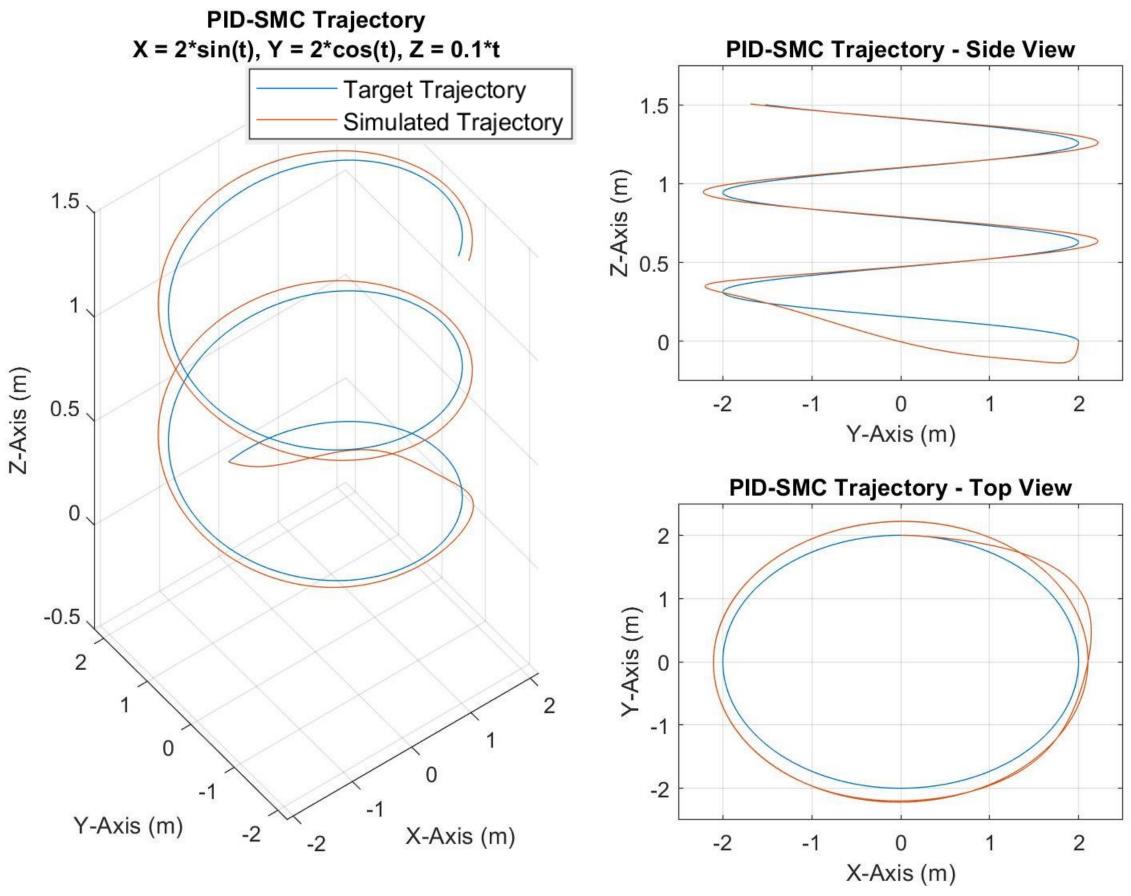


Fig. 5: PID Position Control and SMC Attitude Control. 15s simulation, 50Hz controller frequency

This work shows the feasibility of an NMPC algorithm using weighted basis functions that reduces optimization parameters and increase operating frequency and prediction time. Next, the NMPC algorithm will be thoroughly tuned and evaluated in simulations over more trajectories. Then, it will be implemented on a quadrotor and evaluated experimentally.

S. Khatiwada, A. Masters, A. Cantara, M. Goulet and M.W. Thein. "Control of an Earth-Based Satellite Test Platform through Vision-Based Position Measurement." AAS/AIAA 29th Spaceflight Mechanics Meeting, Hawaii, 2019.

Simulations

Fig. 4: NMPC Position Control and SMC Attitude Control. 15s simulation, 50Hz controller frequency, 2s prediction horizon w/ 10 basis functions per axis

Conclusions and Future Work

References